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SPECTROPHOTOMETRIC ANALYSIS OF AQUEOUS MIXTURES OF SOME CHROMIUM (III) COMPLEXES

(NASA-CR-172999) SPECTROPHOTOMETRIC ANALYSIS OF AQUEOUS MIXTURES OF SOME CHROMIUM (III) COMPLEXES Thesis (Spring Arbor Coll., Mich.) 27 p HC A03/MF A01 CSC1 07D G3/25 15008

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Thesis Submitted in Partial Fulfillment for Honors in Chemistry to the Faculty of Spring Arbor College



by

Gregory Stevens

May, 1983

ACKNOWLEDGEMENTS

The Author wishes to express his sincere gratitude to Dr. David Johnson, advisor, for his guidance and encouragement throughout the entire course of this research. And to Mr. William Bunch for his invaluable assistance and contributions.

The Author also wishes to express his appreciation to Mrs. Elizabeth Shaffer for her laboratory assistance and aid in the collection of experimental data. And especially to Rebekah Rohrer for her continuous encouragement and support.

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SPECTROPHOTONETRIC ANALYSIS OF AQUEOUS MIXTURES OF SOME CHRONIUM (III) COMPLEXES

I. INTRODUCTION

There is a great need for electrical storage development for remote power system applications that are supplied either by solar photovoltaic arrays or wind turbine generators. (1) Lead-acid batteries are currently used for this application but costs are high and the system level is difficult to maintain. (2) Over the past ten years, the NASA-Lewis Research Center has developed the NASA-Redox concept (3,4) to where small but complete Redox energy storage systems have been built. These inexpensive, relatively unsophisticated systems store energy during periods when ample power is being produced by solar or wind generators, and supplied to the various loads during low production periods. (5)

Another application for energy storage systems is in electric utility service where they would serve in a load leveling capacity. (6) These storage devices would be in the ten megawatt size range and would be used on a daily cycle.

The NASA-Redox Energy Storage system is an electrochemical storage device that utilizes the oxidation and reduction of two soluble redox couples for charging and discharging. The active solutions, seperated by a highly selective ion exchange membrane, are pumped through a stack of Redox flow cells where the electrochemical reactions take place at porous carbon felt electrodes. The redox couples currently in use are acidified solutions of chromium {Cr(III)/Cr(II)} and iron {Fe(III)/Fe(II)}.

A diagram showing the single Redox cell and the electrode reactions is

shown in figure 1. The anion exchange membrane seperates the compartments and prevents the cross-mixing of the reactive cations. The electrode material is carbon felt, catalyzed by trace amounts of gold and lead on the chromium side. The need for the catalyst is evident because the rate of reduction of Cr(III) to Cr(II) is slow on most surfaces.(7,8) The catalyst must have a high overvoltage for hydrogen because, thermodynamically, hydrogen is evolved before chromium is reduced. The result of coevolution of hydrogen is a reduction in coulombic efficiency and a loss of balance electrochemically in the system after many cycles. Trace amounts of gold (12 to 25 ug/cm²) and lead (100 to 200 ug/cm²) deposited on the carbon felt meet the criteria for an effective catalyst. The gold produces a surface onto which lead deposits uniformly during a slow charging cycle. No catalyst is required on the iron electrode.

During a discharge cycle, chloride ions move from the cathode compartment to the anode compartment, and hydrogen ions move in the opposite direction. On charge all reactions are reversed.

The relatively inert inner-sphere complex ions $Cr(H_2O)_5Cl^{+2}$ and $Cr(H_2O)_4Cl_2^+$ are present at equilibrium with $Cr(H_2O)_6^{+3}$ in aqueous solutions containing Cr(III) and chloride ion.(9) Both color changes and open-circuit v ltage versus state-of-charge plots confirm the presence of these complex ions. Distinctive differences in the chromium solutions are observed at the same state of charge depending on whether the cell is in the charge or discharge mode, as seen in figure 2. At above 50 percent state-of-charge the charging rate drops off appreciably.

The two species, $Cr(H_2O)_5CI^{+2}$ and $Cr(H_2O)_6^{+3}$, have been identified as present in Redox solutions by ion exchange chromatography and visible spectrophotometry. Spectral data indicates that the concentration of $Cr(H_2O)_5CI^{+2}$ decreases much

more rapidly with increasing state of charge than does the concentration of $Cr(H_2O)_6^{+3}$ indicating that $Cr(H_2O)_5C1^{+2}$ is the predominant species being reduced during the charging cycle. There is a rapid rise in $Cr(H_2O)_5C1^{+2}$ concentration as discharge takes place, and the concentration of $Cr(H_2O)_6^{+3}$ rises only after appreciable $Cr(H_2O)_5C1^{+2}$ is produced. The main electroactive species, then, is pentasquachromium chloride.(10)

 ${\rm Cr}({\rm H_2O})_5{\rm Cl}^{+2}$ is evidently reduced via an inner-sphere chloride bridged electrode reaction and the oxidation of ${\rm Cr}({\rm H_2O})_5{\rm Cl}^+$ as an inner-sphere chloride bridged electrode reaction. A slowly attained equilibrium exists between ${\rm Cr}({\rm H_2O})_6^{+3}$ and ${\rm Cr}({\rm H_2O})_5{\rm Cl}^{+2}$ that is catalyzed by ${\rm Cr}({\rm II}).(10)$

From this information it is crucial that methods be developed to study and control the equilibrium between ${\rm Cr}({\rm H_2O})_5{\rm Cl}^{+2}$ and ${\rm Cr}({\rm H_2O})_6^{+3}$. The ability to control this equilibrium would provide the means to increase the efficiency and capacity of the NASA Redox Energy Storage System.

Increased temperature of the system is believed to thermodynamically shift the equilibrium between the chromium complexes to favor the ${\rm Cr}({\rm H_2O})_5{\rm Cl}^{+2}$ species—the main electroactive species. In order to study this temperature effect reliable methods of chromium analysis and determination are necessary.

This work describes and compares several methods of determining the relative concentrations of ${\rm Cr(H_2O)}_5{\rm Cl}^{+2}$ and ${\rm Cr(H_2O)}_6^{+3}$. The three methods studied are curve resolving methods, used in evaluating spectrophotometric results, mixture studies, used in verifying curve resolving techniques, and chromium analysis.

II. EXPERIMENTAL

All visible spectrophotometric work was done on a Perkin-Elmer Coleman 124 double beam spectrophotometer with a Sargent model SR recorder.

Preparation of $Cr(H_2O)_5C1^{+2}$ and $Cr(H_2O)_6^{+3}$.

Ion exchange chromatography was used to obtain the pure $Cr(H_2O)_5Cl^{+2}$ and $Cr(H_2O)_6^{+3}$.(11) A solution of .07 M $Cr(H_2O)_4Cl_2^{+}$ was prepared by dissolving 4.663 g of $CrCl_2^{+}6H_2O$ in 250 ml of .002 M $HClO_4$. A 38cm x l1mm column was prepared using Dowex 50W-X8 (50-100 mesh) cation exchange resin. The .07 M $Cr(H_2O)_4Cl_2^{+}$ (63°C) was placed on the fresh column and eluted with .1 M $HClO_4$ (approximately 100 ml).

The most weakly held cation, $Cr(H_2O)_4Cl_2^+$, was liberated from the column as a result of the .1 M HClO₄ elution. Upon pouring 1.0 M HClO₄ onto the column $Cr(H_2O)_5Cl^{+2}$ was caused to move down the resin and was collected. Finally, 3.0 M HClO₄ was required to displace the very strongly bound $Cr(H_2O)_6^{+3}$ from the resin. Since we were interested only in the $Cr(H_2O)_5Cl^{+2}$ and $Cr(H_2O)_6^{+3}$ complexes, they were the only two complexes saved for this study.

The visible spectra of the complexes were in agreement with literature values.

Preparation of Standard Chromate solutions used in Chromium Analysis.

A standardized 100 ppm chromium solution in the form of chromate was prepared by dissolving .2829 g Primary Standard $K_2Cr_2O_7$ in 1000.0 ml of standard .05 M KOH. Dilutions were made of this solution to 10 ppm, 7.5 ppm, 6.0 ppm, 3.5 ppm, 2.5 ppm, and 1.0 ppm chromium in the form of chromate ion. Absorbance was read for each diluted solution at 366 mu, using .05 M KOH as

a reference. A graph was constructed plotting concentration (abscissa) vs. absorbance (ordinate).

Preparation of Chromium samples for analysis

In order for appropriate absorption readings to be taken, the chromium complexes must be converted to chromate ion and diluted such that their colors correspond to that of the standard chromate solutions. 2.0 ml of $Cr(H_2O)_5Cl^{+2}$ and 2.0 ml of $Cr(H_2O)_6^{+3}$ were seperately pipetted into a 100 ml volumetric flask. 50 ml of .05 M KOH was added to each flask followed by 8 drops $30^{\frac{1}{2}}H_2O_2$ and then more .05 M KOH to dilute each to 100 ml. The solutions were allowed to stand overnight. 10 ml of each chromate species was diluted to 1000 ml with .05 M KOH, making the total dilution factor from the original solution 1/5000. Absorbance at 366 mu was recorded for each diluted solution.

Mixture Studies

Mixtures of $Cr(H_2O)_5C1^{+2}$ to $Cr(H_2O)_6^{+3}$ were made using the following ratios and volumes: 1:1 (2.0 m1:2.0 m1), 2:1 (4.0 m1:2.0 m1), and 1:2 (2.0 m1:4.0 m1). 2.0 m1 pipettes were used in this procedure. Absorption spectra were obtained for each of these mixtures. Mixtures of 1:1, 2:1, and 1:2 $Cr(H_2O)_5C1^{+2}$ to 0.1 M HClO₄ and 1:1, 2:1, and 1:2 0.1 M HClO₄ to $Cr(H_2O)_6^{+3}$ were prepared and spectra were obtained using 0.1 M HClO₄ as reference.

Curve Resolving

The DuPont 310 Curve Resolver was used to study the absorption curves. It was used to add the component bands of the pure complexes, giving the

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composite band of the mixture.

The 310 Curve Resolver is a special purpose analog computer for the rapid resolution of overlapping peaks in experimental data. To accomplish this, the instrument generates a series of component peaks and synthesizes a sum curve matching the original data. The 310 was set to generate, on each of its function generator channels, peak shapes corresponding to Gaussian distributions. Individual peak parameters of height, width, and horizontal position were varied on each channel until each peak of the individual species spectra was represented by a seperate channel. The desired curves were then summed by switching on and off the appropriate channels to yield the composite curve structure similar to the spectra of the mixtures obtained from the mixture studies.

When working with mixtures in which one or both of the species is very concentrated the curve resolver will not be as accurate near the wavelength of maximum absorbance.

Computer Analysis

All computer work was done on a Radio Shack TRS-80 Level II computer utilizing disk basic.

III. DATA AND CALCULATIONS

Computer Analysis

The absorption spectra of $Cr(H_2O)_5C1^{+2}$ and $Cr(H_2O)_6^{+3}$ and their mixtures are shown in figures 3 thru 5. Molar absorptivities (ϵ) at various wavelengths for the two species were calculated using these spectra and Beer's Law and were used in the computer analysis. They are listed in table 1.

A computer program was developed which computes the concentrations of two species using data from the absorption spectra of the mixture of the two species. The program, SPEC/BAS, is listed in the data section.

A sample run of the program is found in the data section. This program takes data from visible spectra as input and gives concentration of species, standard deviation and relative average deviation as output. It also incorporates a means of not including erroneous values in the calculation of the average concentration of the individual species.

When working with mixtures in which one or both of the species is very dilute (less than .1 M) the computer program SPEC/BAS must be edited to accommodate these values. There is an error factor in line 2040 (underlined in listing of program in data section) which must be increased to a value which will give acceptable output from the computer. The rationale behind this is that in the program there exists a subroutine (lines 2000-2180) which eliminates concentration values which are in error of the mean by a factor greater than the error factor. For very dilute solutions, which are already subject to spectrophotometric errors, a small error factor would cause most of the computed concentrations to be eliminated.

A listing of the solutions to the combinations of linear simultaneous equations is also contained in the output, as well as the total standard deviation and relative average deviation for all of these results, erroneous values included.

The program SPEC/BAS was used to analyze the absorption curves of the three mixtures of chromium complexes. The results are shown in table 2 in tabular form.

Chromium Analysis

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The plot of absorbance vs. concentration for chromium is shown in figure 6. The diluted $Cr(H_2O)_5Cl^{+2}$ had an absorbance reading of 0.342, which corresponds to a concentration of 3.80 ppm, according to the calibration curve. Knowing the dilution factor to be 1/5000, the original sample concentration is calculated to be 0.365 M $Cr(H_2O)_5Cl^{+2}$. The chromium complex $Cr(H_2O)_6^{+3}$ had an absorbance value of 0.760, corresponding to 0.813 M.

With this information, the concentrations of the chromium complexes used in the mixture studies can be calculated. The concentrations computed for this study are listed in table 2.

Curve Resolving

The summations of the individual component curves using the Curve Resolver are shown in figures 3 thru 5. The summation curve from the Curve Resolver accurately matches the absorption bands of the chromium complex mixture. The greatest error was found near the wavelength of maximum absorbance (λ_{max}) , where the discrepancy between the mixture's absorbance and the Curve Resolver's results is as much as 5.0% for one peak. The mean discrepancy at λ_{max} was 1.7% for the peak whose maximum occurs near 585 mu and 2.3% for the peak whose maximum occurs near 415 mu.

λ_{max} Correlation

Figure 7 illustrates the plot of wavelength of maximum absorbance (abscissa) vs. concentration ratio (mole fraction) of $Cr(H_2O)_6^{+3}/\{Cr(H_2O)_5Cl^{+2} + Cr(H_2O)_6^{+3}\}$ (ordinate). It is interesting to note that a linear relationship is found between absorbance and concentration ratio (mole fraction $Cr(H_2O)_6^{+3}$).

IV. DISCUSSION

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The computer program gave very good results for the determination of chromium complex ion concentrations from the analyzation of the chromium complex mixture's spectra data. Table 2 shows the percent errors of the mean values using the concentrations determined from the chromium analysis as the accurate standard values. The concentration values from the chromium analysis are within the expected error of the standard deviations for the computer analysis for the mixture ratios 1:1 and 2:1 $\text{Cr}(\text{H}_2\text{O})_5\text{Cl}^{+2}$ to $\text{Cr}(\text{H}_2\text{O})_6^{+3}$. This is not the case for the 1:2 mixture ratio, however. These errors are due, presumably, to a number of factors: molar absorptivity calculation errors, and absorbance errors due to a combination of wavelength errors in the spectrophotometer and large slopes of the absorption curves

The curve resolving proved to provide an accurate means of representing absorption curves using a Gaussian-type distribution. The summation curve errors occurring near the wavelength of maximum absorption were due to the extreme sensitivity of the Curve Resolver near the peaks of the curves. In addition, it must be taken into account that absorption curves are only similar to Gaussian-type distributions and can not be represented exactly by this type of a curve similation.

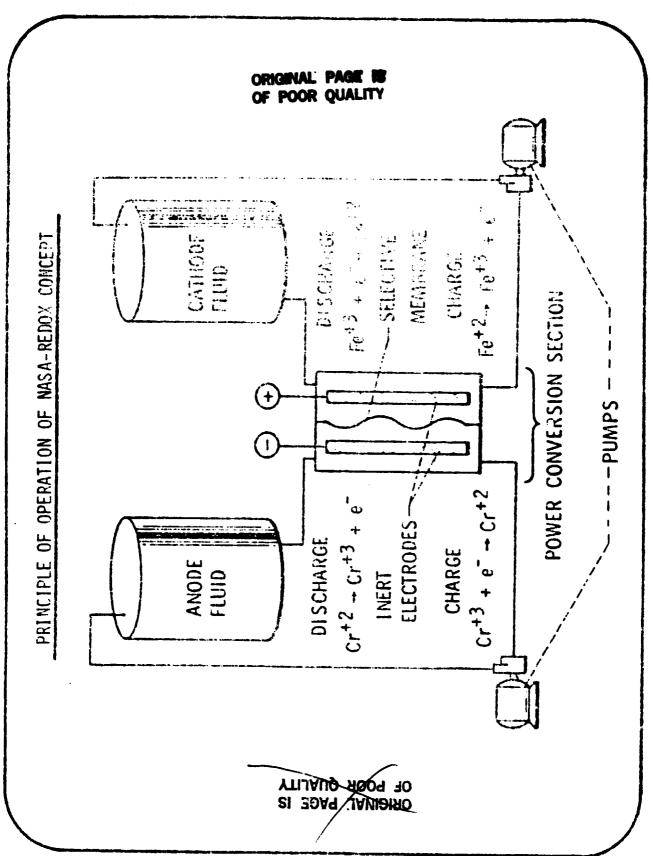
V. CONCLUSION

Several methods for determining the concentrations of $\mathrm{Cr}(\mathrm{H}_2\mathrm{O})_5\mathrm{Cl}^{+2}$ and $\mathrm{Cr}(\mathrm{H}_2\mathrm{O})_6^{+3}$ in aqueous solutions containing $\mathrm{Cr}(\mathrm{III})$ and chloride ion were found to provide valuable results. Curve resolving was found to provide an excellent means of resolving spectra of mixtures of $\mathrm{Cr}(\mathrm{H}_2\mathrm{O})_5\mathrm{Cl}^{+2}$ and $\mathrm{Cr}(\mathrm{H}_2\mathrm{O})_6^{+3}$

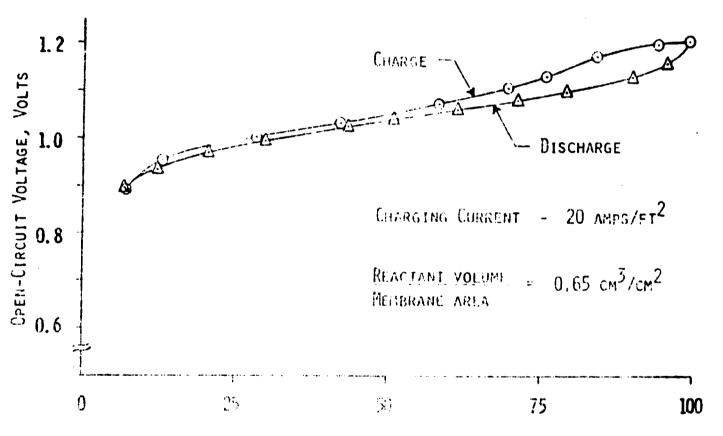
into their individual component absorption spectra. The chromium analysis studies proved to be very reliable and presented a method of evaluating the curve resolving and computer analysis.

Future applications for these methods of study can be seen in the area of temperature studies on the Cr(III) solution. Studies of this type would determine the potential of utiliqing the heat generated by the Redox Energy Storage System's pumps to increase the temperature of the electrolyte solutions. Increased temperature of the system is believed to have the effect of shifting the equilibrium between the chromium complexes to favor $\text{Cr}(\text{H}_2\text{O})_5\text{Cl}^{+2}$ --the electroactive species. Should this effect occur, the electrical capacity and efficiency of the system would increase.

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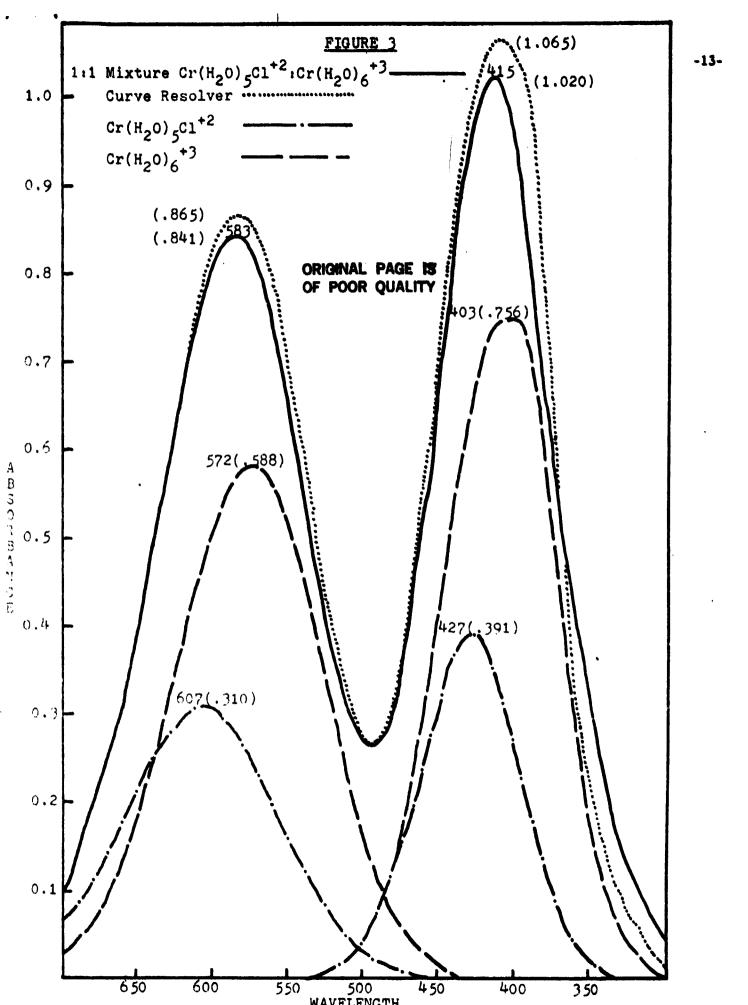


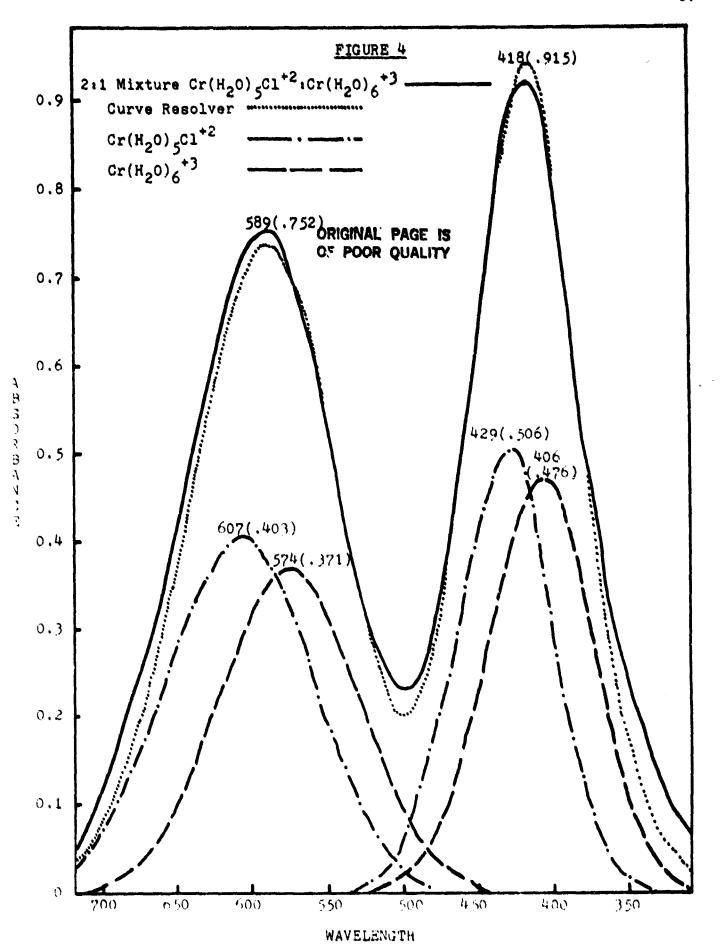
OPEN-CIRCUIT VOLTAGE HYSTERESIS OF IRON/CHROMIUM REDOX CELL



STATE-OF-CHARGE, PERCENT

FIGURE 2







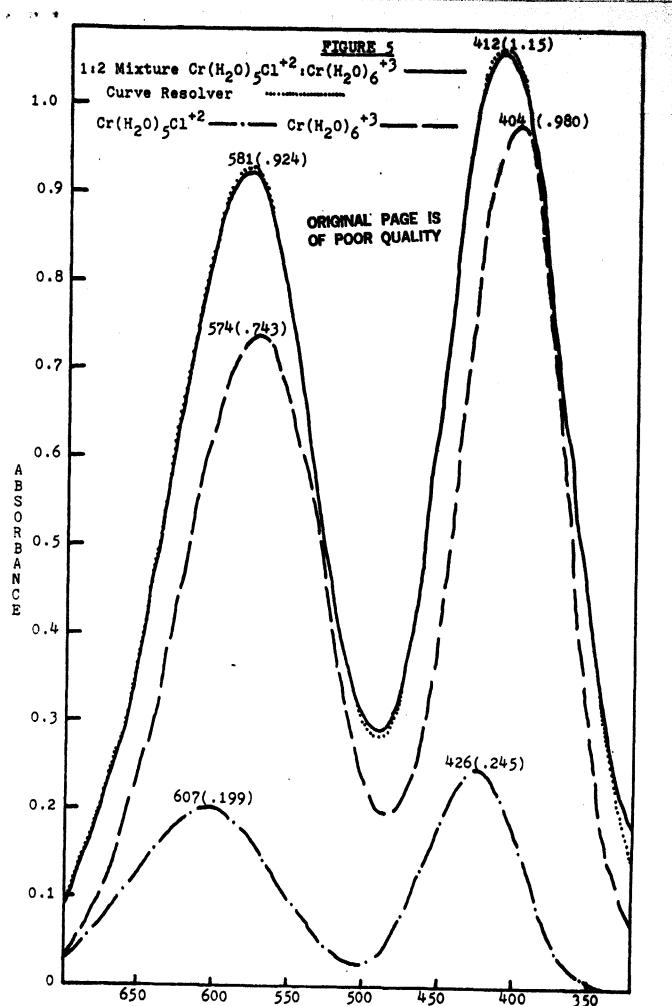
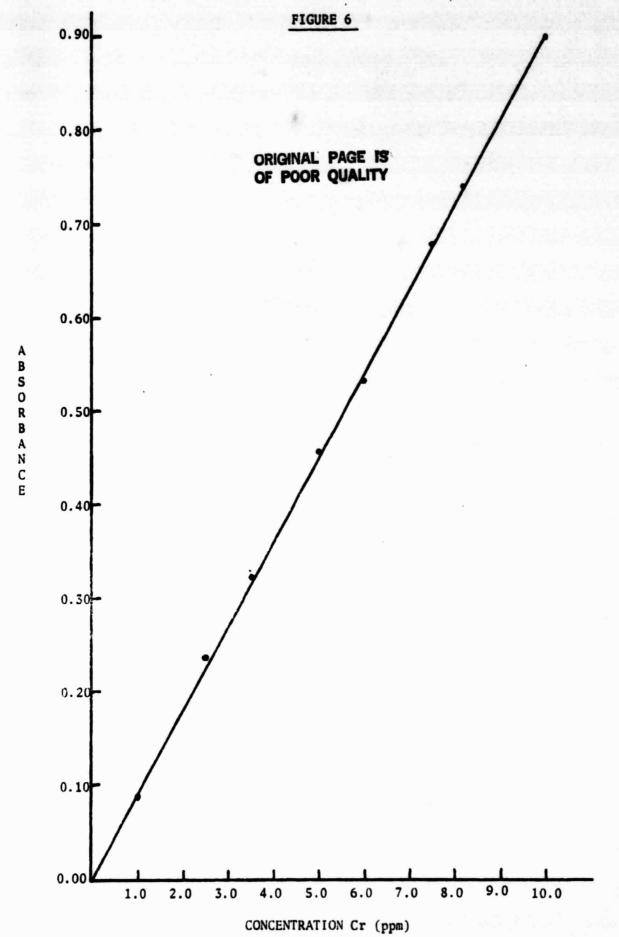
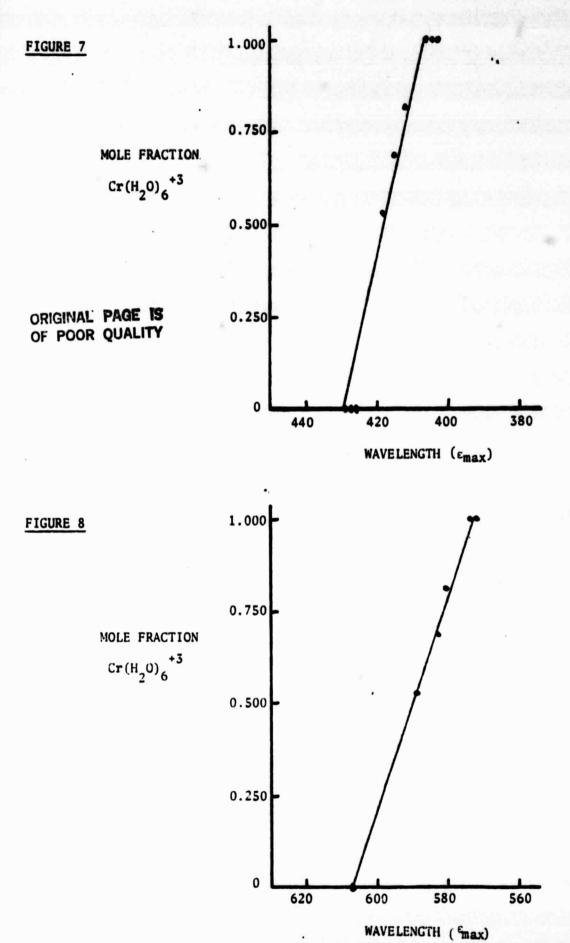


	TABLE 1	
Wavelength	E cr(H20)5C1+2	€cr(H20)6+3
652	11.15	3.76
628	15.05	7.30
592	15.66	13.06
556	8.93	12.81
532	5.04	8.96
460	13.21	6.28
442	18.91	10.58
418	19.62	16.93
388	7.78	16.16
370	2.58	11.93

	TABLE 2		
Mixture Ratio	Concentration (M) from SPEC/BAS	Concentration (M) from Cr Analysis	% Error
Cr(H ₂ 0) ₅ C1 ⁺² Cr(H ₂ 0) ₆ ⁺³	0.200 <u>+</u> .019	0.183	8.5
1:1 Cr(H ₂ 0) ₆ +3	0.399 ±.026	0.407	2.0
2:1 Cr(H ₂ 0) ₅ C1 ⁺² Cr(H ₂ 0) ₆ ⁺³	0.255 <u>+</u> .020	0.243	4.7
Cr(H ₂ 0) ₆ ⁺³	0.272 ±.022	0.271	0.4
1:2 Cr(H ₂ 0) ₅ C1 ⁺² Cr(H ₂ 0) ₆ +3	0.145 ±.013	0.122	15.8
1:2 Cr(H ₂ O) ₆ +3	0.517 ±.020	0.542	4.8







SAMPLE RUN OF THE COMPUTER PROGRAM "SPEC/BAS"

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50 PRINTS38 - SOLUTION USING UV-VIS SPECTROSCOPY DATA - 1
 78 PRINTS914. "HIT ANY KEY TO CONTINUE"
88 29-INKEYSIIF 29-" THEN 88 ELSE 98
 90 2501
100 LPRINT' DETERMINATION OF CONCENTRATIONS OF TWO SPECIES'
130 LPRINT' IN SOLUTION USING UV-VIS SPECTROSCOPY DATA'
148 LPRINT' 150 LPRINT
 140 LPRINT ":LPRINT" 145 GOTO 3808
 175 CLS
180 PRINT "ENTER THE NUMBER OF HAVELENGTHS FROM HHICH"
190 PRINT "DATA IS TAKEN"
280 INPUT D
210 IF D<2 THEN 220 ELSE 235
220 PRINT YOU MUST ENTER AT LEAST 2 HAVELENGTHS."
  238 GOTO 182
235 CLS
248 GOSUB 4888
  245 CLE
  250 E=D-1
260 DIM W(D)+A(D)+M(D+2)+B(D)+C(D+D+2)+SD(2+2)+RAD(2+2)+F(2)+G(2)
  278 FOR I=1 TO D
288 PRINT'ENTER WAVELENGTH #"11
  290 INPUT W(I)
  310 PRINT'ENTER ADSORBANCE AT WAVELENGTH" (W())
  320 INPUT A(I)
  330 PRINT**
340 PRINT*ENTER MOLAR ABSORPTIVITY OF FIRST*
  350 PRINT" COMPONENT AT WAVELENGTH" : W(I)
  360 INPUT M(1+1)
  380 PRINT'ENTER MOLAR ABSORPTIVITY OF SECOND'
  390 PRINT COMPONENT AT WAVELENGTH : W(1)
             INPUT M(1.2)
   400
  410
              PRINT'ENTER THE CELL WITH USED (IN CM)"
   420
   430 INPUT B(1)
   440
              CLS
              PRINT PLEASE WAIT
   445
  ASO NEXT I
   468 REM
                                    PRINTED OUTPUT OF DATA
   470 LPRINT WAVELENGTH . . ABSORBANCE . . MOLAR ABSORPTIVITY 1.2".
             LPRINT CELL HIDTH
   480
   498 LPRINT
   510 50----
   528 He="#. #"
   530 FOR 1=1 TO D
548 LPRINT TAB(4) W(1):
  SSE LPRINT TAB(19):LPRINT USING FS:A(I):

SAB LPRINT TAB(35):LPRINT USING GS:M(I:1):

S78 LPRINT TAB(48):LPRINT USING GS:M(I:2):

575 LPRINT **
   SEC LPRINT USING HEIR(I)
   STO NEXT I
   595 REM
                                   COMPUTATIONS
    680 N-0
   618 5(1)=8
   628 $(2)=8
638 K=2:E=D-1
648 FORI=1 TO E
658 FORJ=K TO D
```

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### C(1+2+1)=(A(1)+M(2+2)-A(2++M(1+2))/(B(1)+(M(1+1)+M(1+2)+M(1+2)+M(1+2)+M(1+1))/
678 C(1,J;2)=(A(J)+M(I;1)-A(I)+M(J;1))/(B(I)+(M(I;1)+M(J;2)-M(I;2)-M(I;2))
680 B(I)=B(I)+C(I;J;1)
690 B(I)=B(I)+C(I;J;2)
                                                                                                                                          -22-
780 N=N+1
718 NEXT J
728 KWK+1
738 IF K=(D=1) THEN 750
748 MEYT 1
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758 Y=8(1)/M
760 VAR/21/14
                                                                                OF POOR QUALITY
770 '=INT(>=18866+.5)/18868
788 '=INT(>=18866+.5)/18868
783 606UE 2000
798 REM PRINT OUTPUT CONCENTRATIONS 888 LPPINT" " *LPRINT" *
BIS LPRINT" THE CONCENTRATION OF THE FIRST SPECIES IS "IX! "HOLAP"
828 LPRINT'
838 LPRINTITIE CONCENTRATION OF THE SECOND SPECIES IS VICTOLAR'S ST. LERINT "FILPRINT"
840 LPRINT'FIPS: SPECIES STANDARD DEVIATION IS "FILPRINT USING POFF(1)
ESO LPRINT SECOND SPECIES STANDARD DEVIATION IS "TILPRINT USING FEIFTS
955 LPRINT
eg: Rem. Standard Deviation and Relative average Deviation
SIE LPRINTSCONCENTRATION PLAS CONCENTRATION WE
715 LPRINT.
1858 N3-N3-1
1188 BD(1+1)=(C(1+J+1)=X1+2
1118 BD(2+1)=BD(1+1)+BD(2+1)
1128 RAD(1-1) -A88(C(1-J-1)-X)
1170 RAD(2:1)=RAD(1:1)=RAD(2:1)
1140 8D(1:2)=(C(1:J:2)=Y112
1188 8D(2-2)=8D(1-2)=8D(2-2)
1168 RAD(1-2)=A88(C(1-J-2)-Y)
1178 RAD(2-2)=RAD(1-2)+RAD(2-2)
1200 NEXT J
1218 KeK+1
1228 IF H=(D+1) THEN 1245
1238 NEXT 1
1248 LPRINT" "ILPRINT"THERE HERE INDITOTAL PAIRS OF CONCENTRATION COMPARISONS!
1245 N2WN
1245 N2WN
1256 IF N<2 THEN N=2
1255 IF N<2 THEN N=2
1256 X2=K1Y2=Y
1257 IF YOU OR YOU THEN X-1:Y-1
1268 #(1)=(SD(2+1)/(N-1))+.5
1278 G(1)=(RAD(2:1)/((N-1)-K))+188
1288 F(2)=(BD(2:2)/(N-1))+.5
1298 5(2)#(RAD(2-2)/((N-1)#Y))#180
1292 N=N2
1293 X=X2:Y=Y2
1295 LPRINT* *1LPRINT* *
1300 LPRINTTHERS WERETINITSIMULTANEOUS EQUATIONS UMED FOR THE CONCENTRATION DETERMINATIONS
1218 LPPINT
TITLE CHAINTITY TOTAL STANDARD DEVIATION FOR FIRST SPECIES IS "TELLPRINT USING FETEL)
TOTAL STANDARD DEVIATION FOR ECOND SPECIES IS TELLPRINT USING FETEL
TOTAL STANDARD DEVIATION FOR ECOND SPECIES IS TELLPRINT USING FETE
12 ( .....
12-0 LERINT'T TAL RELATIVE ANGRADE DENIATION FOR FIRRT BRECIES IS FRURRINT VEING SPECI OF NUPETHATION AND SPECIES IS FRURRINT VEING SPECI OF NUPETHATION AND SPECIES IS FRURRINT VEING SPECIATION FOR SECOND SPECIES IS FRURRINT VEING GRAND FRURTHING LABOUR FURTHAND AND THE PROGRAM AGAIN VES OR NOTIZE
1417 IF DESCREEN THEN LIPSTAT CHES 12/16/17/2
1430 FOR 1446TOERISET(1:18:INEXT
1440 FOR 1858*044 ETER -115ET(1+15)1NE)T
1450 FOR 1812TO18 STER -115ET 44+1)1NE(T 1
1450 IF 184*NOT PRINTSCES+THANK YOUTLESE PRINTSCES+TRY AGAINT
1460 IF 14-"NO" PR
1470 PPINT8-900-
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1480 FOR 1=: TO3000 INEXT

1490 1F28="NO" THEN 9000 ELSE 1400

156

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                                                                                                                     OF POOR QUALITY
  2135 N-N2
2148 X-INT(X-18080-.5)/18088
2158 Y-INT(Y-18080-.5)/18088
  2150 Y=INT(Y=18080+.5)/18080
2163 L=L+1
2170 IF L=10 THEN 2190
2180 SOTO 2812
2190 RETURN
3000 REM INPUT TITLE
2803 CLEAR 64
3818 INPUT "ENTER THE TITLE: "1T6
3820 LPRINT T6
3830 LPRINT" ":LBRINT" "
3840 GOTO 178
4860 REM COMPUTE SD AND RAD FOR REMAINING VALUES
4820 SD:(1.1)=C((I.J.1)-X1+2
4830 SD:(2.1)=SD:(1.1)+SD:(2.1)
4840 RAD:(1.1)=RAD:(2.1)
4840 RAD:(1.1)=RAD:(2.1)
4840 SD:(1.2)=(C(I.J.2)-Y)+2
GN3 608P
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